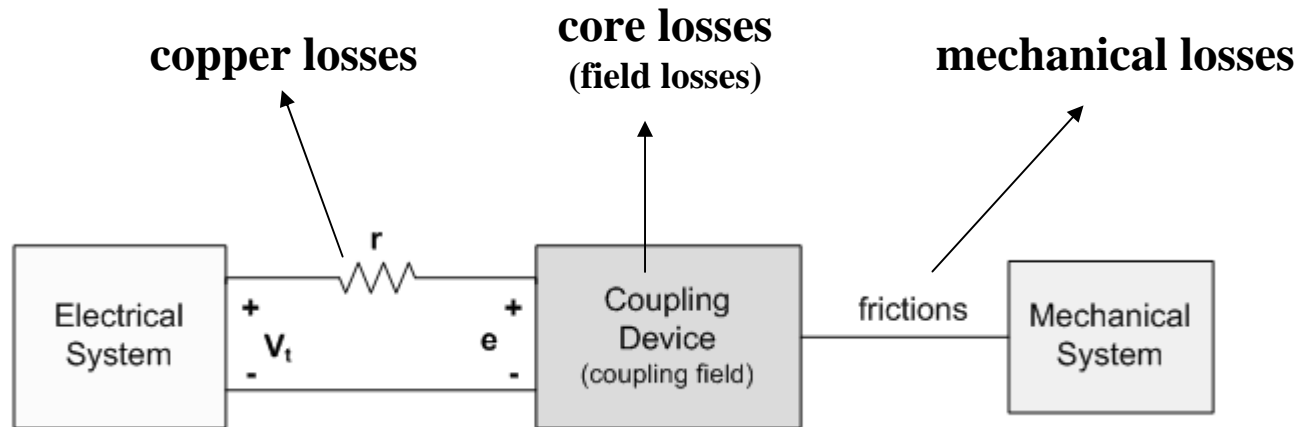


III. Electromechanical Energy Conversion

Schematic representation of an electromechanical energy conversion device



Differential energy input from electrical source:

$$dW_{elec} = V_t i dt - i^2 R dt = e i dt$$

$$dW_{mech} = \text{net mechanical energy output} + \text{mechanical losses}$$

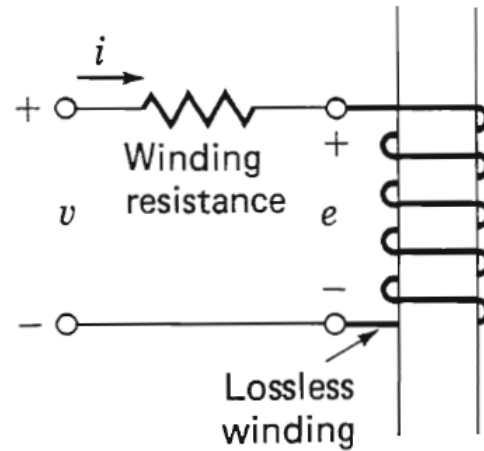
Differential energy balance eqn.:

$$dW_{elec} = dW_{mech} + dW_{fld} + \text{field losses}$$

For a lossless magnetic energy storage system:

$$dW_{elec} = dW_{mech} + dW_{fld}$$

1. Energy in Magnetic Field



$$dW_{elec} = ei dt$$

$$dW_{elec} = N \frac{d\phi}{dt} idt$$

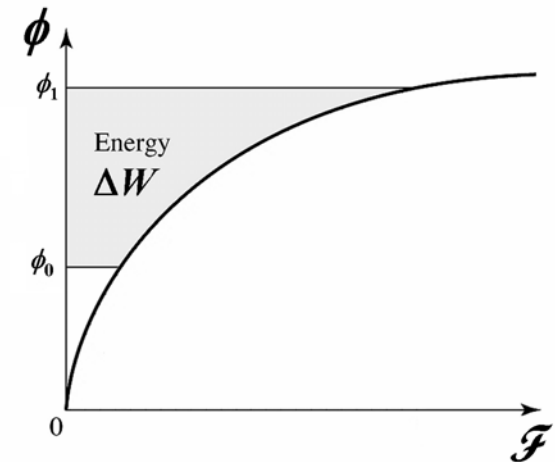
$$dW_{elec} = Nid\phi$$

$$dW_{elec} = \mathcal{F} d\phi$$

$$W_{elec} = \int_{\phi_0}^{\phi_1} \mathcal{F} d\phi$$

$$= W_{fld}$$

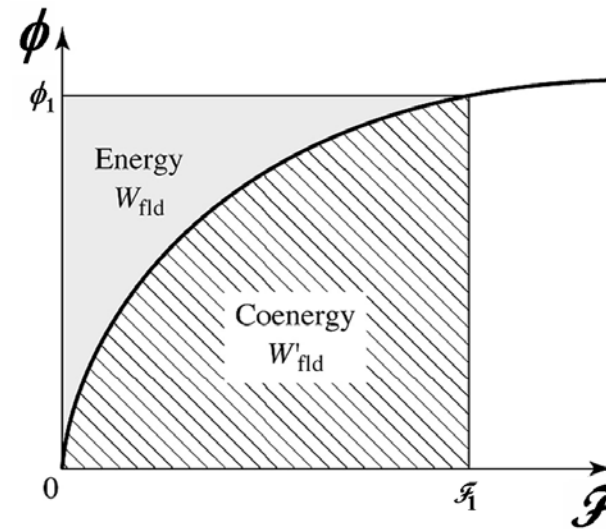
$$= \int_0^{\phi_1} \mathcal{F} d\phi - \int_0^{\phi_0} \mathcal{F} d\phi$$



Coenergy

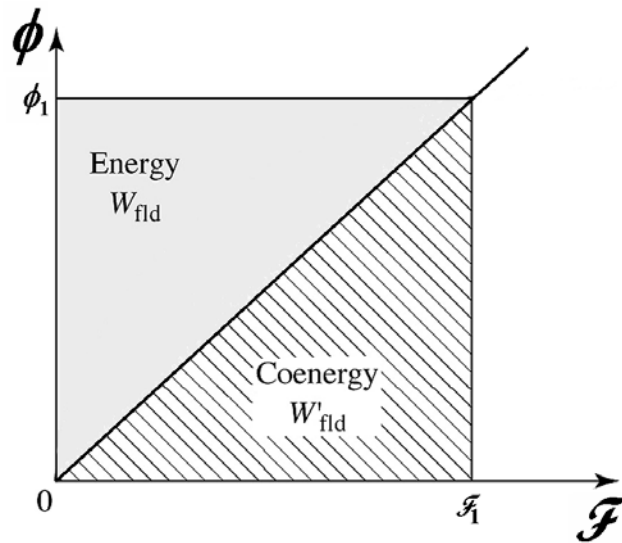
with $\phi_0 = 0$ and $\mathcal{F}_0 = 0$

$$W'_{fld} = \int_0^{\mathcal{F}_1} \phi \, d\mathcal{F}$$



$$W_{fld} + W'_{fld} = \mathcal{F}_1 \phi_1$$

For a linear magnetic circuit:



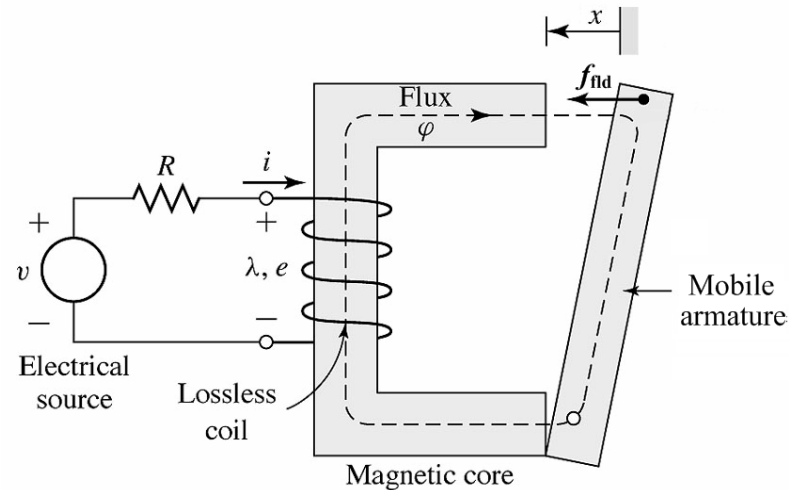
$$W_{fld} = W'_{fld} = \frac{1}{2} \mathcal{F}_1 \phi_1$$

$$= \frac{1}{2} \mathcal{R} \phi_1^2$$

$$= \frac{1}{2} \mathcal{P} \mathcal{F}_1^2$$

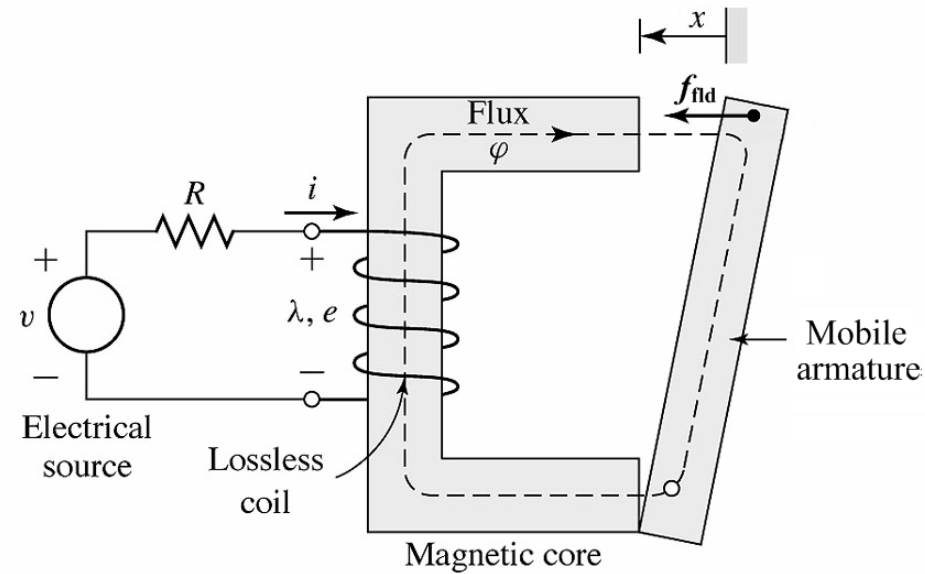
where \mathcal{R} and \mathcal{P} are the reluctance and permeance of the magnetic circuit respectively

2. Energy & Force in Singly-Excited E.M.C device



Electromechanical relay

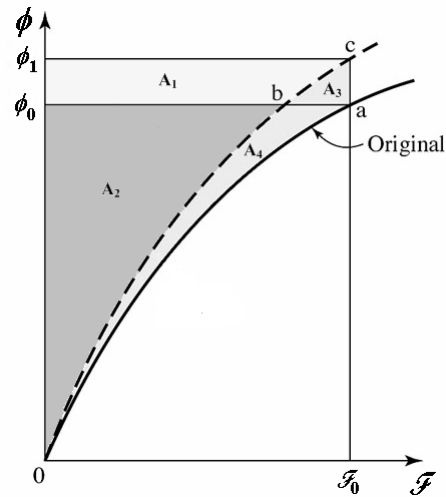
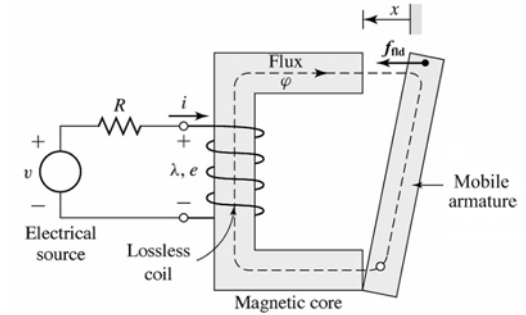
- Assume mobile armature is initially at open position
- When the coil is excited by $i(t)$, $\phi(t)$ is produced in M.C. and an electromagnetic force f_{fld} is exerted on mobile armature tending to align it with the densest part of M.F.
- When the armature moves $\phi \uparrow$



Armature Movement

- Slow motion case (ϕ is gradually increased during motion)
- Fast motion case (ϕ is constant during motion)
- Normal motion case

(i) Slow motion



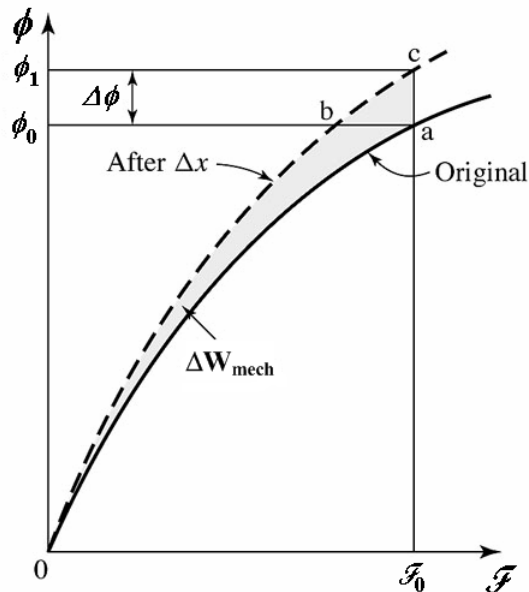
$$\Delta W_{elec} = \Delta W_{fld} + \Delta W_{mech}$$

$$\Delta W_{elec} = \int_{\phi_0}^{\phi_1} \mathcal{F} d\phi = A_1 + A_3$$

$$\Delta W_{fld} = \int_0^{\phi_1} \mathcal{F} d\phi - \int_0^{\phi_0} \mathcal{F} d\phi = (A_1 + A_2) - (A_2 + A_4)$$

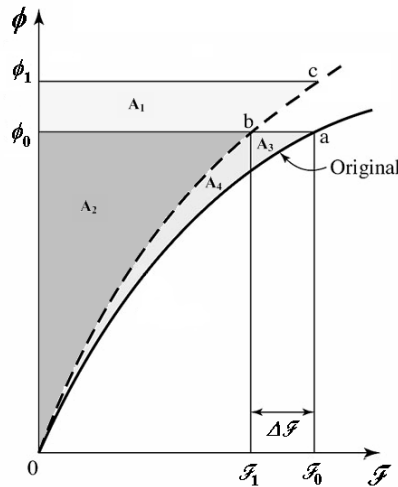
\mathcal{F} is constant during motion

$$\Delta W_{mech} = \Delta W_{elec} - \Delta W_{fld} = A_3 + A_4$$

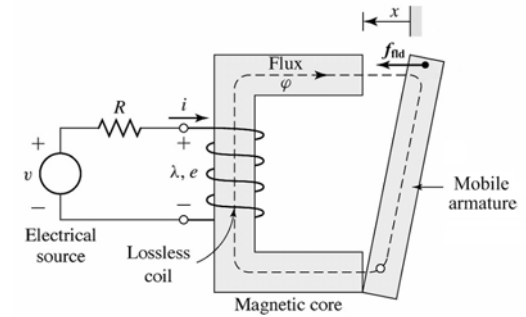
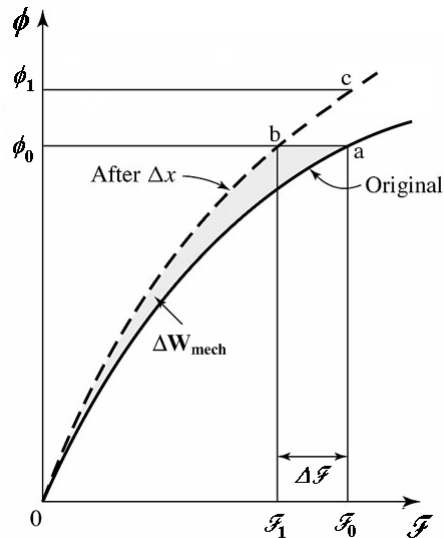


← Shaded area gives ΔW_{mech}

(ii) Fast motion



ϕ is constant during motion



$$\Delta W_{elec} = \Delta W_{fld} + \Delta W_{mech}$$

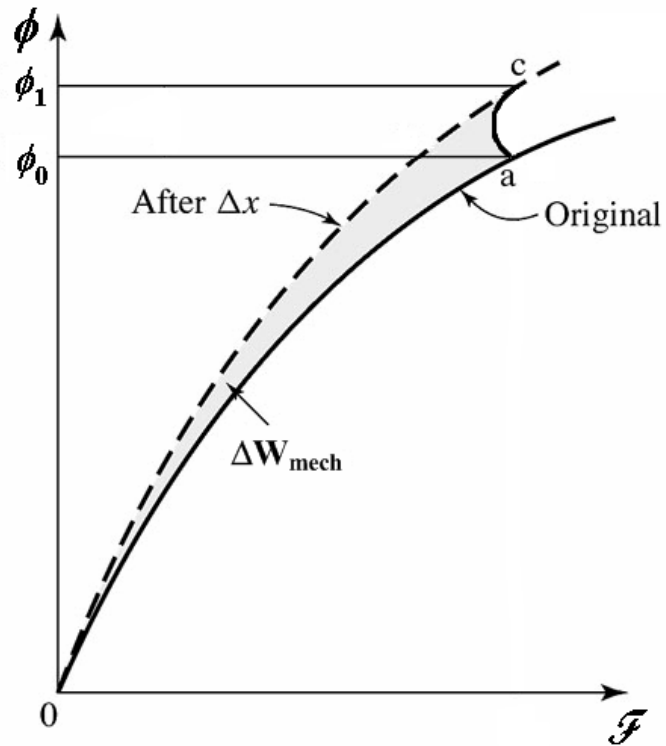
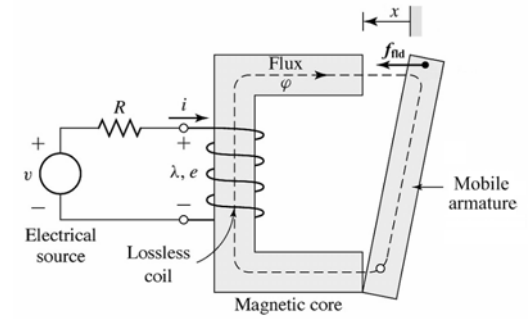
$$\Delta W_{elec} = \int_{\phi_0}^{\phi_1} \mathcal{F} d\phi = A_1$$

$$\Delta W_{fld} = \int_0^{\phi_1} F d\phi - \int_0^{\phi_0} F d\phi = (A_1 + A_2) - (A_2 + A_3 + A_4)$$

$$\Delta W_{mech} = \Delta W_{elec} - \Delta W_{fld} = A_3 + A_4$$

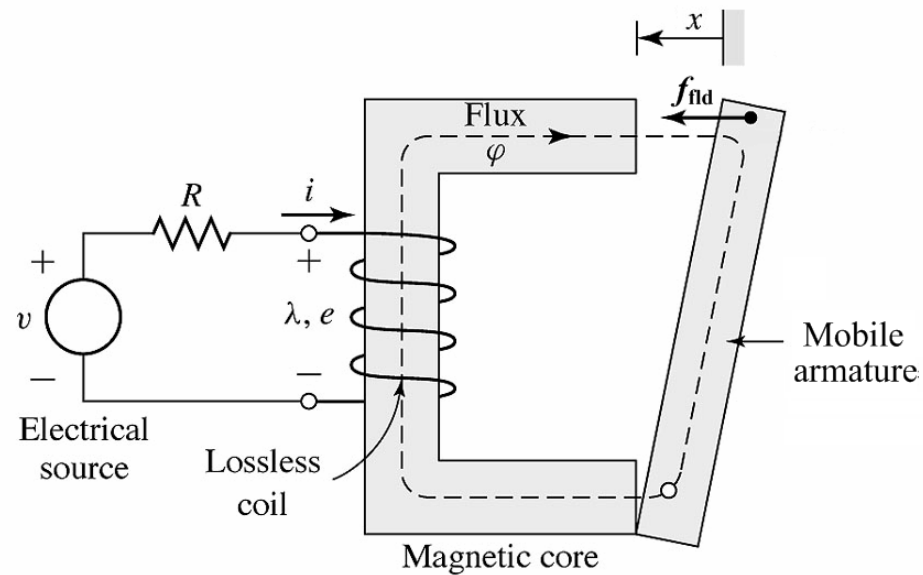
← Shaded area gives ΔW_{mech}

(iii) Normal motion



$$\Delta W_{elec} = \Delta W_{fld} + \Delta W_{mech}$$

← Shaded area gives ΔW_{mech}



$$dW_{mech} = f_{fld} dx$$

- if $dW_{mech} > 0$ then electrical system does work on the armature
- if $dW_{mech} \leq 0$ then mechanical system does work on the armature

(a) Mechanical force in fast motion

$$dW_{elec} = dW_{fld} + dW_{mech}$$

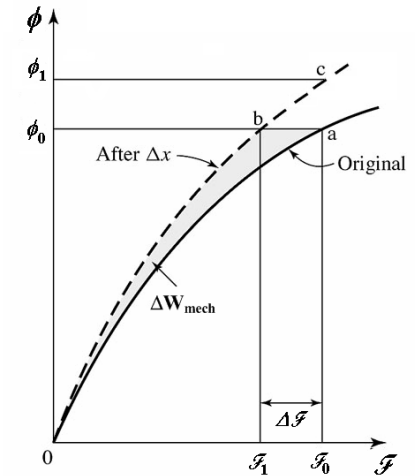
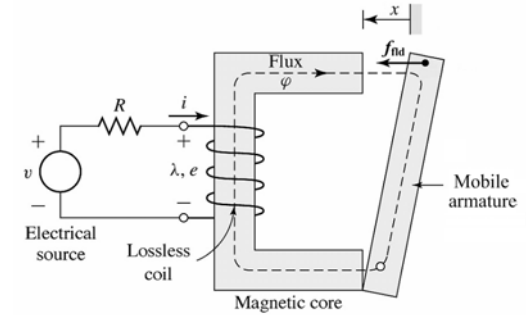
$$\mathcal{F} d\phi = dW_{fld} + f_{fld} dx$$

$$dW_{fld} = \mathcal{F} d\phi - f_{fld} dx$$

Note that
$$dW_{fld}(\phi, x) = \frac{\partial W_{fld}(\phi, x)}{\partial \phi} d\phi + \frac{\partial W_{fld}(\phi, x)}{\partial x} dx$$

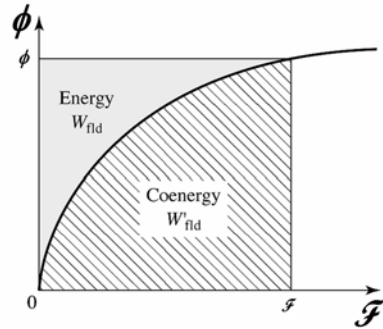
So
$$\mathcal{F} = \frac{\partial W_{fld}(\phi, x)}{\partial \phi}$$

and
$$f_{fld} = -\frac{\partial W_{fld}(\phi, x)}{\partial x}$$



ϕ is independent of x

(a) Mechanical force in slow motion



$$W'_{fld}(\mathcal{F}, x) = \mathcal{F} \phi - W_{fld}(\mathcal{F}, x)$$

$$dW'_{fld}(\mathcal{F}, x) = d(\mathcal{F} \phi) - dW_{fld}(\mathcal{F}, x)$$

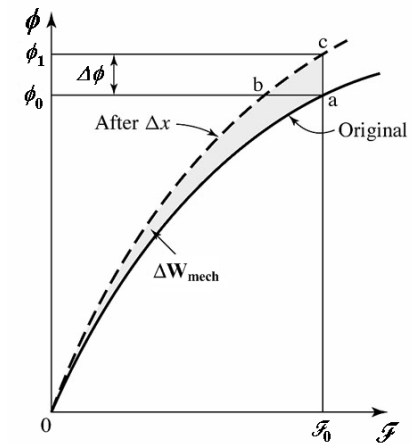
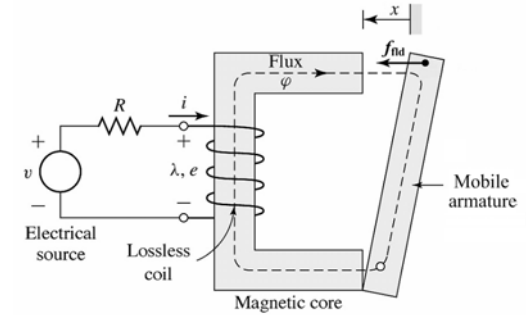
$$dW'_{fld}(\mathcal{F}, x) = \phi d\mathcal{F} + \mathcal{F} d\phi - (\mathcal{F} d\phi - f_{fld} dx)$$

$$\boxed{dW'_{fld}(\mathcal{F}, x) = \phi d\mathcal{F} + f_{fld} dx}$$

Note that
$$dW'_{fld}(\mathcal{F}, x) = \frac{\partial W'_{fld}(\mathcal{F}, x)}{\partial \mathcal{F}} d\mathcal{F} + \frac{\partial W'_{fld}(\mathcal{F}, x)}{\partial x} dx$$

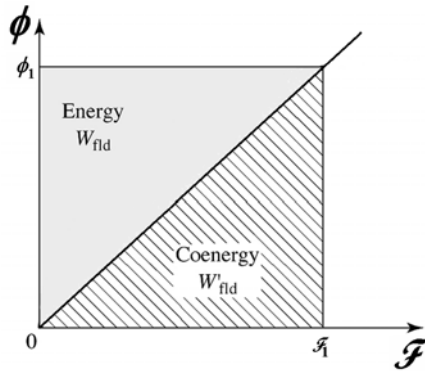
So
$$\boxed{\phi = \frac{\partial W'_{fld}(\mathcal{F}, x)}{\partial \mathcal{F}}}$$

and
$$\boxed{f_{fld} = \frac{\partial W'_{fld}(\mathcal{F}, x)}{\partial x}}$$



\mathcal{F} is independent of x

For a linear magnetic circuit



$$W_{fld} = W'_{fld} = \frac{1}{2} \mathcal{F} \phi = \frac{1}{2} \mathcal{R} \phi^2 = \frac{1}{2} \mathcal{P} \mathcal{F}^2$$

where \mathcal{R} and \mathcal{P} are the reluctance and permeance of the magnetic circuit respectively

1. When ϕ is constant during motion

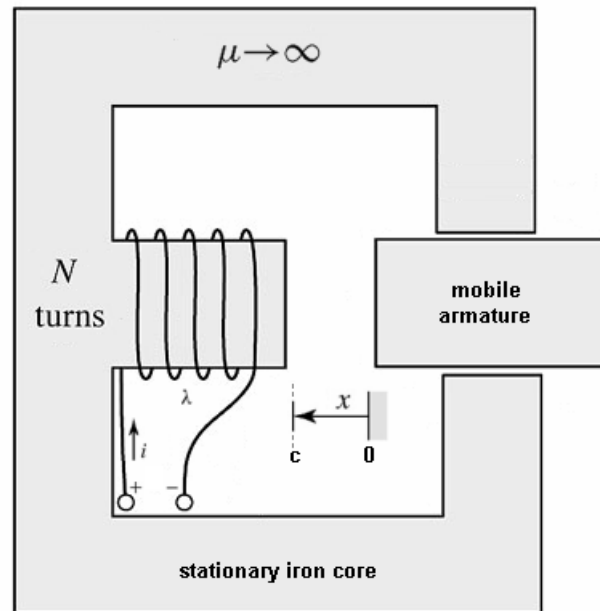
$$f_{fld} = -\frac{1}{2} \phi^2 \frac{d\mathcal{R}}{dx}$$

2. When \mathcal{F} is constant during motion

$$f_{fld} = \frac{1}{2} \mathcal{F}^2 \frac{d\mathcal{P}}{dx} = \frac{1}{2} i^2 \frac{dL}{dx}$$

Ex-1: Derive an expression for the electromagnetic force f_{fld} produced by the E.M.D. shown in the figure and then plot f_{fld} against x .

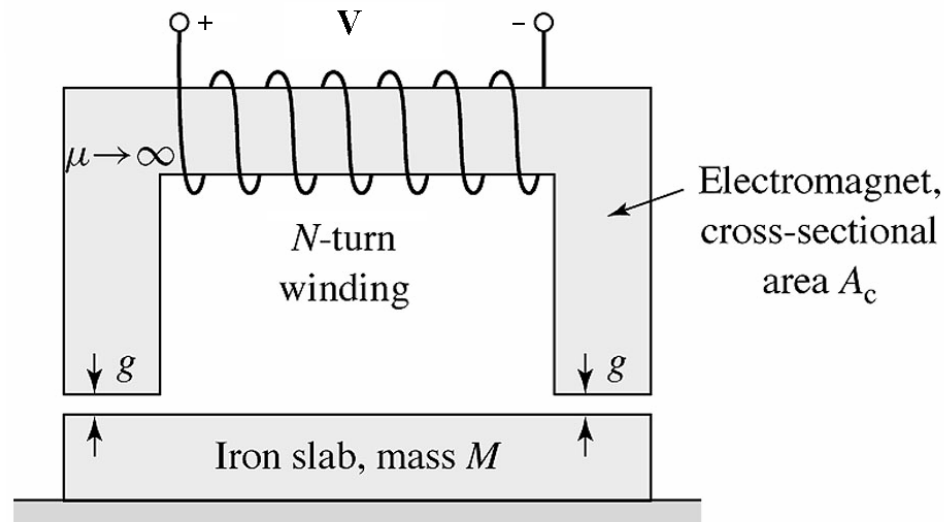
Note: Initial gap length is c and i is constant during motion



Ex-2: For the electromagnet shown below:

- (a) For $V = 120 \text{ Vdc}$, determine the energy stored in magnetic field and the lifting force produced
- (b) For $V = 120 \text{ Vac}$ at 60 Hz, determine the average lifting force produced

Note: Initial gap length is 5 mm, internal resistance of the winding $r = 6\Omega$, $N = 300$, $A_c = A_g = 6 \times 6 = 36 \text{ cm}^2$.



3. Rotating Machines

Linear Motion	Linear Displacement $x, \text{ m}$	Linear Speed $v, \text{ m/s}$	Mass $m, \text{ kg}$	Force $f, \text{ N}$
Rotational Motion	Angular Displacement $\theta, \text{ rad}$	Angular Speed $\omega, \text{ rad/s}$	Inertia $J, \text{ kg m}^2$	Torque $T_e, \text{ Nm}$

fast motion

$$f_{fld} = -\frac{\partial W_{fld}(\phi, x)}{\partial x}$$

For flux independent of θ during motion:

$$\Rightarrow T_e = -\frac{\partial W_{fld}(\phi, \theta)}{\partial \theta}$$

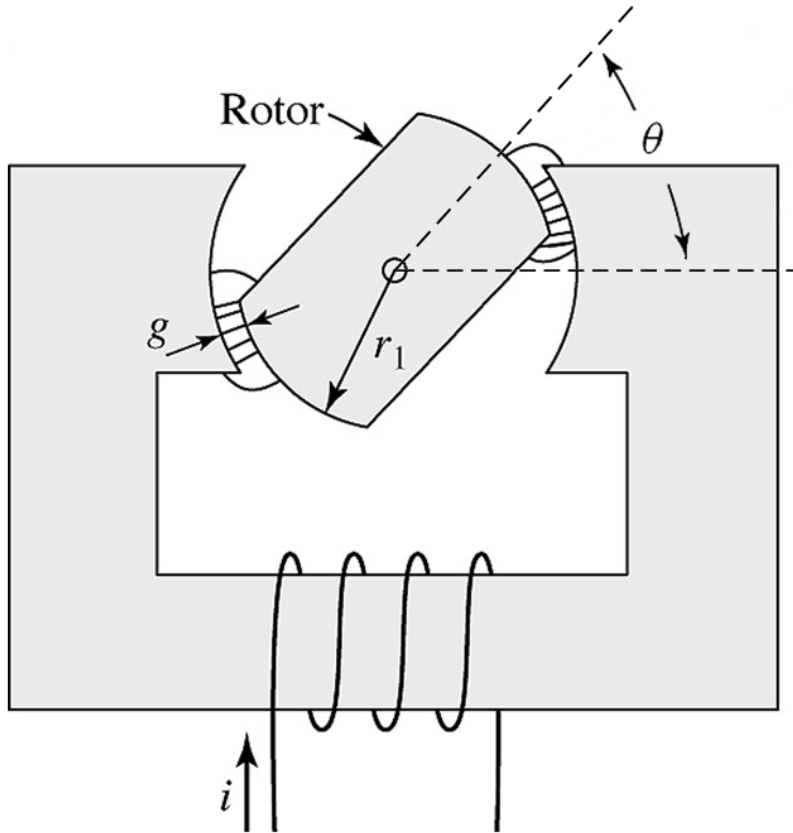
slow motion

$$f_{fld} = \frac{\partial W'_{fld}(\mathcal{F}, x)}{\partial x}$$

For mmf independent of θ during motion:

$$\Rightarrow T_e = \frac{\partial W'_{fld}(\mathcal{F}, \theta)}{\partial \theta}$$

(a) Singly-excited device



$$\theta = \omega_r t + \theta_0$$

For a linear M.C.

$$T_e = \frac{1}{2} i^2 \frac{dL}{d\theta}$$

$$P_{mech} = T_e \omega_r \quad \omega_r = \frac{d\theta}{dt}$$

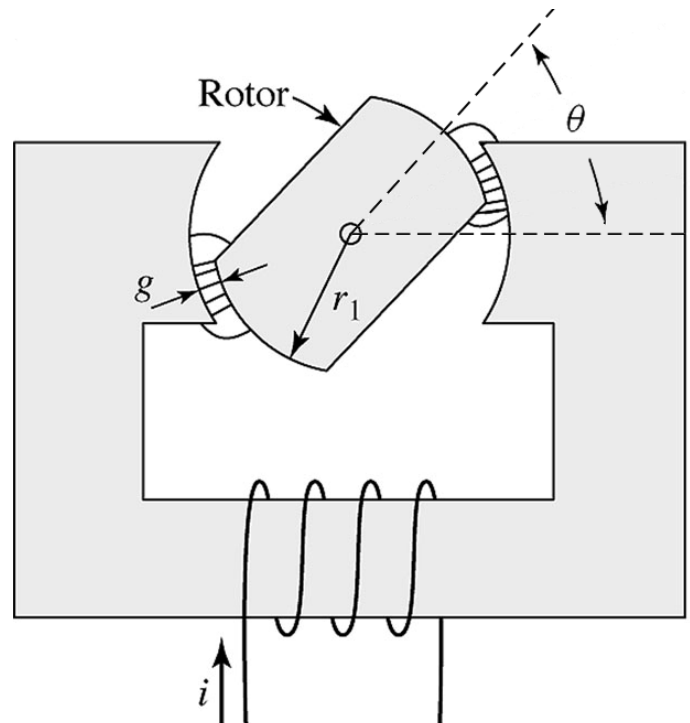
$$P_{mech} = \frac{1}{2} i^2 \frac{dL}{dt}$$

Ex: The self inductance $L(\theta)$ in the figure as a function of rotor position is given by

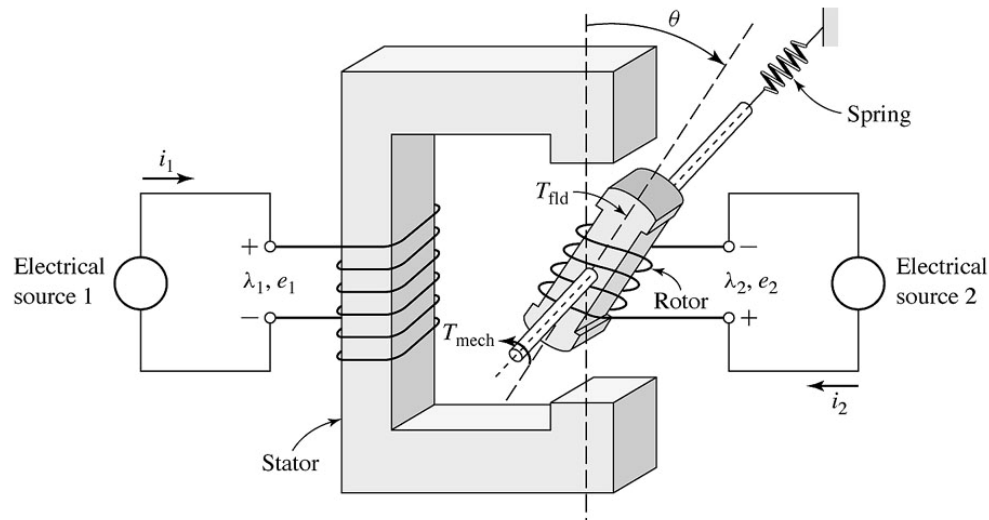
$$L(\theta) = L_0 + L_2 \cos(2\theta)$$

where the stator current is $i(t) = I_m \sin(\omega t)$

- (i) Obtain an expression for electromagnetic torque produced (instantaneous torque)
- (ii) Let $\theta = \omega_1 t + \theta_0$, find necessary condition for non-zero average torque



(b) Doubly-excited device



$$\lambda_1 = L_1 i_1 + M i_2$$

$$\lambda_2 = L_2 i_2 + M i_1$$

$$\lambda_1 = L_1(\theta) i_1(t) + M(\theta) i_2(t)$$

$$\lambda_2 = L_2(\theta) i_2(t) + M(\theta) i_1(t)$$

$$e_1 = \frac{d\lambda_1}{dt} \quad e_2 = \frac{d\lambda_2}{dt}$$

$$e_1 = L_1 \frac{di_1}{dt} + i_1 \frac{dL_1}{d\theta} \frac{d\theta}{dt} + M \frac{di_2}{dt} + i_2 \frac{dM}{d\theta} \frac{d\theta}{dt}$$

$$e_2 = L_2 \frac{di_2}{dt} + i_2 \frac{dL_2}{d\theta} \frac{d\theta}{dt} + M \frac{di_1}{dt} + i_1 \frac{dM}{d\theta} \frac{d\theta}{dt}$$

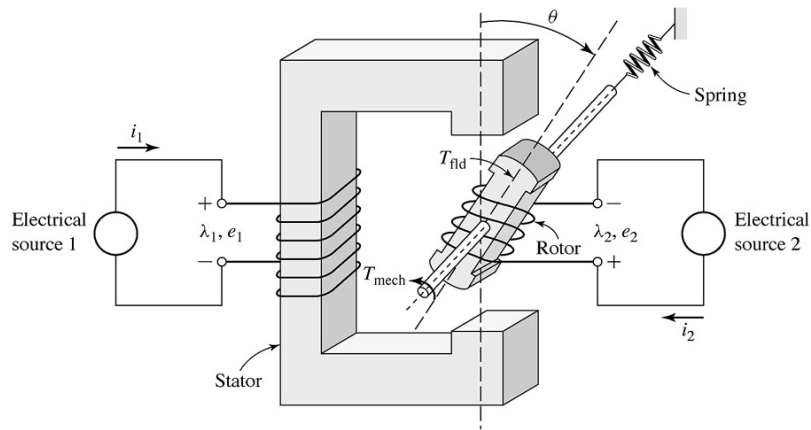
$$v_1 = e_1 + r_1 i_1$$

$$v_2 = e_2 + r_2 i_2$$

$$\omega_r = \frac{d\theta}{dt}$$

Terminal voltage equation (in matrix form):

$$\begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} r_1 & 0 \\ 0 & r_2 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} + \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix} \frac{d}{dt} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} + \frac{d}{d\theta} \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} \omega_r$$



$$\begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} r_1 & 0 \\ 0 & r_2 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} + \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix} \frac{d}{dt} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} + \frac{d}{d\theta} \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} \omega_r$$

Total power $v_1 i_1 + v_2 i_2 = \begin{bmatrix} i_1 & i_2 \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$

$$v_1 i_1 + v_2 i_2 = \mathbf{I}^T \mathbf{V} = \mathbf{I}^T \mathbf{R} \mathbf{I} + \mathbf{I}^T \mathbf{L} \frac{d\mathbf{I}}{dt} + \mathbf{I}^T \frac{d\mathbf{L}}{d\theta} \mathbf{I} \omega_r \quad (\text{in matrix form})$$

P_{elec}

P_{cu}

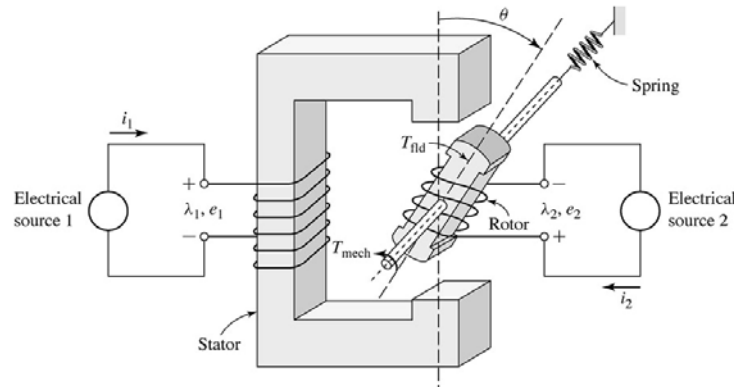
Total electrical power input:

$$P_{elec} = \underbrace{i_1^2 r_1 + i_2^2 r_2}_{\text{Copper loss}} + \underbrace{L_1 i_1 \frac{di_1}{dt} + M i_1 \frac{di_2}{dt} + L_2 i_2 \frac{di_2}{dt} + M i_2 \frac{di_1}{dt} + i_1^2 \frac{dL_1}{d\theta} \omega_r + 2i_1 i_2 \frac{dM}{d\theta} \omega_r + i_2^2 \frac{dL_2}{d\theta} \omega_r}_{\text{Rate of increase in stored energy in MF + Electr.power converted to mech. en.}}$$

Copper loss

Rate of increase in stored energy in MF + Electr.power converted to mech. en.

$$P_{elec} = i_1^2 r_1 + i_2^2 r_2 + L_1 i_1 \frac{di_1}{dt} + M i_1 \frac{di_2}{dt} + L_2 i_2 \frac{di_2}{dt} + M i_2 \frac{di_1}{dt} + i_1^2 \frac{dL_1}{d\theta} \omega_r + 2i_1 i_2 \frac{dM}{d\theta} \omega_r + i_2^2 \frac{dL_2}{d\theta} \omega_r$$



Magnetic stored energy

$$\begin{aligned} W_{fld} &= \int i_1 d\lambda_1 + \int i_2 d\lambda_2 \\ &= \frac{1}{2} L_1 i_1^2 + \frac{1}{2} L_2 i_2^2 + M i_1 i_2 \end{aligned}$$

$$P_{fld} = \frac{dW_{fld}}{dt}$$

$$P_{fld} = L_1 i_1 \frac{di_1}{dt} + M i_1 \frac{di_2}{dt} + L_2 i_2 \frac{di_2}{dt} + M i_2 \frac{di_1}{dt} + \frac{1}{2} i_1^2 \frac{dL_1}{d\theta} \omega_r + \frac{1}{2} i_2^2 \frac{dL_2}{d\theta} \omega_r + i_1 i_2 \frac{dM}{d\theta} \omega_r$$

$$P_{mech} = P_{elec} - P_{cu} - P_{fld}$$

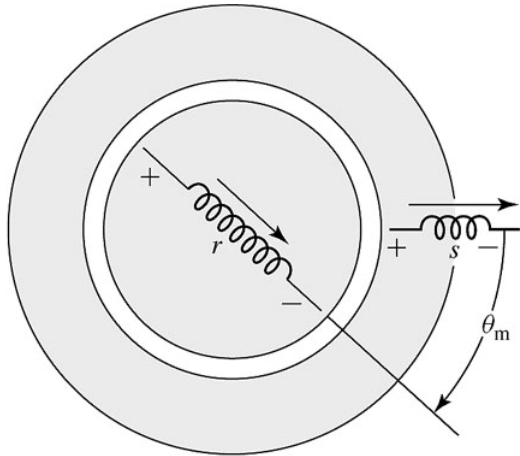
$$P_{mech} = \frac{1}{2} i_1^2 \frac{dL_1}{d\theta} \omega_r + \frac{1}{2} i_2^2 \frac{dL_2}{d\theta} \omega_r + i_1 i_2 \frac{dM}{d\theta} \omega_r$$

$$P_{mech} = T_e \omega_r$$

$$T_e = \frac{1}{2} i_1^2 \frac{dL_1}{d\theta} + \frac{1}{2} i_2^2 \frac{dL_2}{d\theta} + i_1 i_2 \frac{dM}{d\theta}$$

In matrix form: $T_e = \frac{1}{2} \mathbf{I}^T \frac{d\mathbf{L}}{d\theta} \mathbf{I}$

Ex1: T_e ?



Ex2: T_e ?

