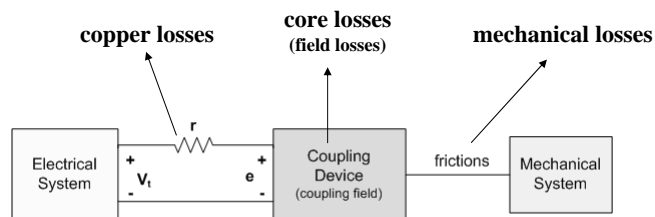# III. Electromechanical Energy Conversion

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Schematic representation of an
electromechanical energy conversion device

Differential energy input from electrical source:

$$dW_{elec} = V_t i\, dt - i^2 R dt = ei\, dt$$

$$dW_{mech} = \text{net mechanical energy output } + \text{ mechanical losses}$$
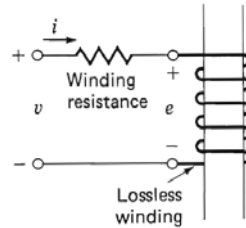
Differrential energy balance eqn.:

$$dW_{elec} = dW_{mech} + dW_{fld} + \text{ field losses}$$

For a lossless magnetic energy storage system:

$$dW_{elec} = dW_{mech} + dW_{fld}$$

1. Energy in Magnetic Field

$$dW_{elec} = ei\,dt$$
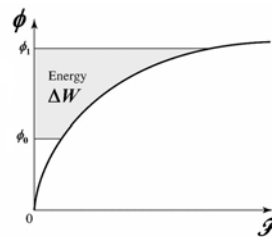
$$dW_{elec} = N\frac{d\phi}{dt}idt$$

$$dW_{elec} = Nid\phi$$

$$dW_{elec} = \mathcal{F}\,d\phi$$

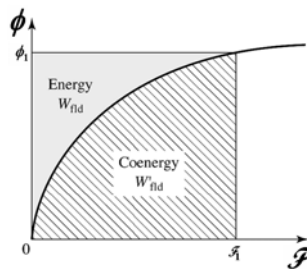$$W_{elec} = \int_{\phi_0}^{\phi_1} \mathcal{F}\,d\phi$$

$$= W_{fld}$$

$$= \int_0^{\phi_1} \mathcal{F}\,d\phi - \int_0^{\phi_0} \mathcal{F}\,d\phi$$
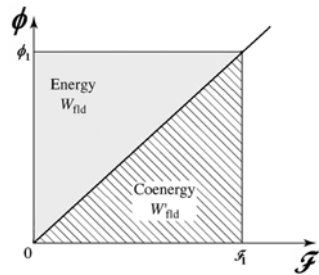

Coenergy

with $\phi_0 = 0$ and $\mathcal{F}_0 = 0$

$$W'_{fld} = \int_0^{\mathcal{F}_1} \phi\,d\mathcal{F}$$

$$W_{fld} + W'_{fld} = \mathcal{F}_1\,\phi_1$$
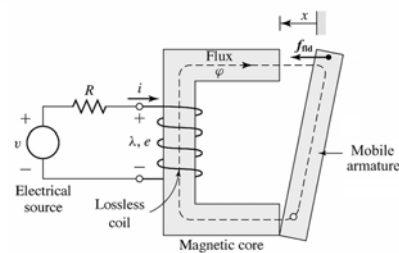
For a linear magnetic circuit:

$$W_{fld} = W'_{fld} = \frac{1}{2}\mathscr{F}_1 \phi_1$$

$$= \frac{1}{2}\mathscr{R}\,\phi_1^2$$

$$= \frac{1}{2}\mathscr{P}\mathscr{F}_1^2$$

where $\mathscr{R}$ and $\mathscr{P}$ are the reluctance and permeance of the magnetic circuit respectively

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# 2. Energy & Force in Singly-Excited E.M.C device

Electromechanical relay

• Assume mobile armature is initially at open position

• When the coil is excited by $i(t)$, $\phi(t)$ is produced in M.C. and an electromagnetic force f_{fld} is exerted on mobile armature tending to align it with the densest part of M.F.
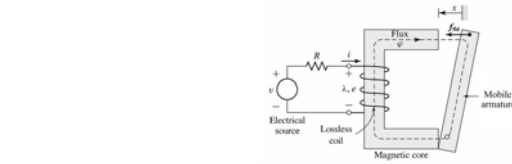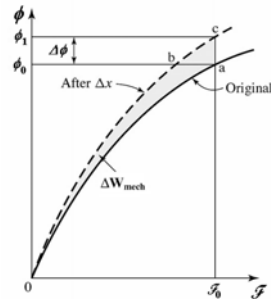
• When the armature moves $\phi\uparrow$
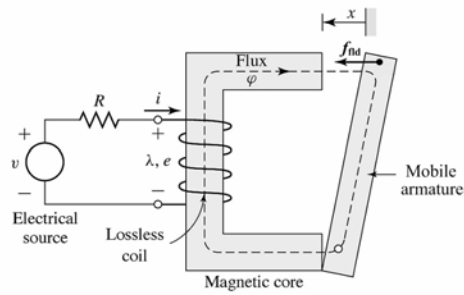
Armature Movement

- Slow motion case   (ϕ is gradually increased during motion)

- Fast motion case   (ϕ is constant during motion)

- Normal motion case

(i) Slow motion
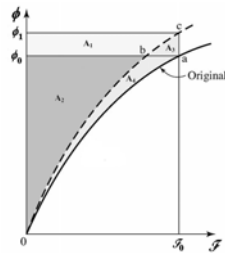
$$\Delta W_{elec} = \Delta W_{fld} + \Delta W_{mech}$$
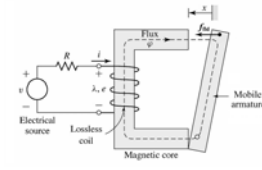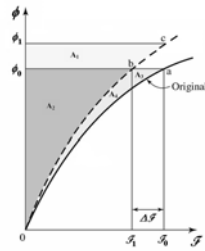
$$\Delta W_{elec} = \int_{\phi_0}^{\phi_1} \mathcal{F}\, d\phi = A_1 + A_3$$

$$\Delta W_{fld} = \int_0^{\phi_1} \mathcal{F}\, d\phi - \int_0^{\phi_0} \mathcal{F}\, d\phi = (A_1 + A_2) - (A_2 + A_4)$$

$\mathcal{F}$ is constant during motion $\Delta W_{mech} = \Delta W_{elec} - \Delta W_{fld} = A_3 + A_4$

$\longleftarrow$ Shaded area gives ΔW_{mech}

(ii) Fast motion

$$\Delta W_{elec} = \Delta W_{fld} + \Delta W_{mech}$$

$$\Delta W_{elec} = \int_{\phi_0}^{\phi_1} \mathcal{F} \, d\phi = A_1$$

$$\Delta W_{fld} = \int_0^{\phi_1} \mathrm{F} \, d\phi - \int_0^{\phi_0} \mathrm{F} \, d\phi = \left(A_1 + A_2\right) - \left(A_2 + A_3 + A_4\right)$$

$$\Delta W_{mech} = \Delta W_{elec} - \Delta W_{fld} = A_3 + A_4$$

ϕ is constant during motion
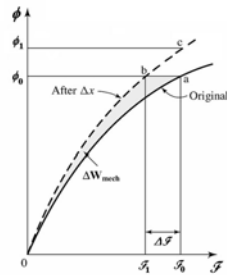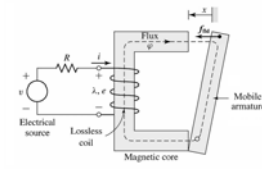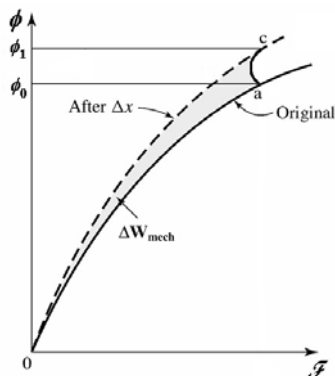

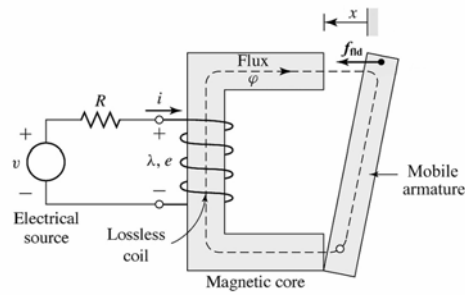⟵ Shaded area gives ΔW_{mech}

(iii) Normal motion

$$\Delta W_{elec} = \Delta W_{fld} + \Delta W_{mech}$$

⟵ Shaded area gives ΔW_{mech}

$$dW_{mech} = f_{fld}\,dx$$

- if $dW_{mech} > 0$ then electical system does work on the armature

- if $dW_{mech} \leq 0$ then mechanical system does work on the armature

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(a) Mechanical force in fast motion

$$dW_{elec} = dW_{fld} + dW_{mech}$$

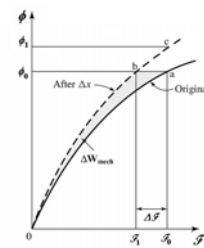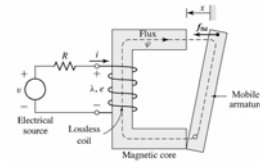$$\mathcal{F}\,d\phi = dW_{fld} + f_{fld}\,dx$$

$$dW_{fld} = \mathcal{F}\,d\phi - f_{fld}\,dx$$

Note that
$$dW_{fld}(\phi, x) = \frac{\partial W_{fld}(\phi, x)}{\partial \phi}\,d\phi + \frac{\partial W_{fld}(\phi, x)}{\partial x}\,dx$$
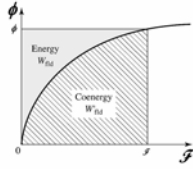
So
$$\mathcal{F} = \frac{\partial W_{fld}(\phi, x)}{\partial \phi}$$

and
$$f_{fld} = -\frac{\partial W_{fld}(\phi, x)}{\partial x}$$

ϕ is independent of x

(a) Mechanical force in slow motion

$$W'_{fld}(\mathcal{F},x) = \mathcal{F}\phi - W_{fld}(\mathcal{F},x)$$

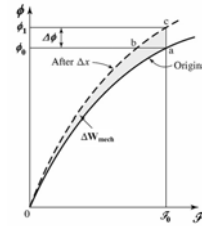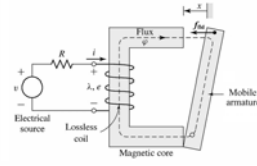$$dW'_{fld}(\mathcal{F},x) = d(\mathcal{F}\phi) - dW_{fld}(\mathcal{F},x)$$

$$dW'_{fld}(\mathcal{F},x) = \phi\, d\mathcal{F} + \mathcal{F}\, d\phi - (\mathcal{F}\, d\phi - f_{fld}\, dx)$$

$$\boxed{dW'_{fld}(\mathcal{F},x) = \phi\, d\mathcal{F} + f_{fld}\, dx}$$

Note that $\quad dW'_{fld}(\mathcal{F},x) = \dfrac{\partial W'_{fld}(\mathcal{F},x)}{\partial \mathcal{F}}\, d\mathcal{F} + \dfrac{\partial W'_{fld}(\mathcal{F},x)}{\partial x}\, dx$

So $\quad \boxed{\phi = \dfrac{\partial W'_{fld}(\mathcal{F},x)}{\partial \mathcal{F}}}$

$\mathcal{F}$ is independent of x

and $\quad \boxed{f_{fld} = \dfrac{\partial W'_{fld}(\mathcal{F},x)}{\partial x}}$

For a linear magnetic circuit
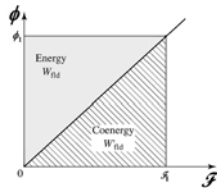
$$W_{fld} = W'_{fld} = \frac{1}{2}\mathcal{F}\phi = \frac{1}{2}\mathcal{R}\phi^2 = \frac{1}{2}\mathcal{P}\mathcal{F}^2$$

where $\mathcal{R}$ and $\mathcal{P}$ are the reluctance and permeance of the magnetic circuit respectively

1. When ϕ is constant during motion

$$\boxed{f_{fld} = -\frac{1}{2}\phi^2 \frac{d\mathcal{R}}{dx}}$$

2. When $\mathcal{F}$ is constant during motion

$$\boxed{f_{fld} = \frac{1}{2}\mathcal{F}^2 \frac{d\mathcal{P}}{dx} = \frac{1}{2}i^2 \frac{dL}{dx}}$$

Ex-1: Derive an expression for the electromagnetic force f_{fld} produced by the E.M.D. shown in the figure and then plot f_{fld} against x.

Note: Initial gap length is c and i is constant during motion
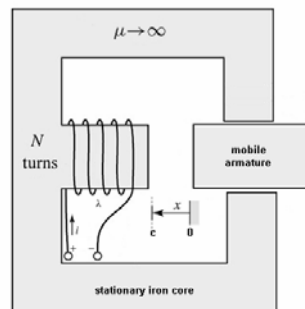
Ex-2: For the electromagnet shown below:
  (a) For $V = 120$ Vdc, determine the energy stored in magnetic field and the lifting force produced
  (b) For $V = 120$ Vac at 60 Hz, determine the average lifting force produced

Note: Initial gap length is 5 mm, internal resistance of the winding $r = 6\Omega$, $N = 300$, $A_c = A_g = 6 \times 6 = 36$ cm^2.

3. Rotating Machines

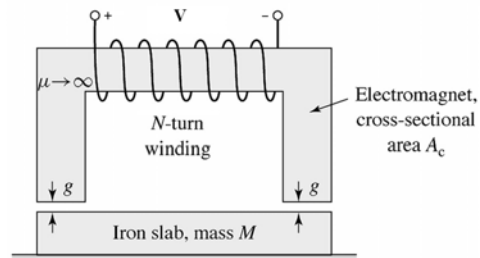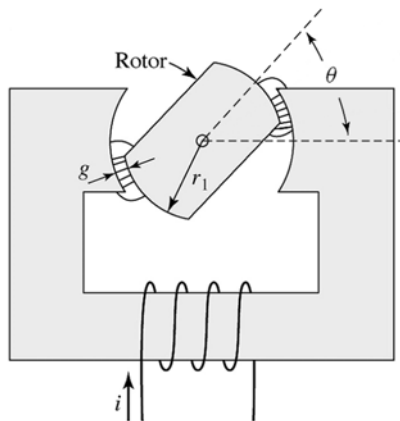|	Linear Displacement	Linear Speed	Mass	Force
Linear Motion	x, m	v, m/s	m, kg	f, N
Rotational Motion	Angular Displacement θ, rad	Angular Speed ω, rad/s	Inertia J, kg m^2	Torque T_e, Nm

For flux independent of θ during motion:

fast motion $\qquad f_{fld} = -\dfrac{\partial W_{fld}(\phi,x)}{\partial x} \qquad \Rightarrow \qquad \boxed{T_e = -\dfrac{\partial W_{fld}(\phi,\theta)}{\partial \theta}}$

For mmf independent of θ during motion:

slow motion $\qquad f_{fld} = \dfrac{\partial W'_{fld}(\mathcal{F},x)}{\partial x} \qquad \Rightarrow \qquad \boxed{T_e = \dfrac{\partial W'_{fld}(\mathcal{F},\theta)}{\partial \theta}}$

(a) Singly-excited device

$$\theta = \omega_r t + \theta_0$$

For a linear M.C.

$$\boxed{T_e = \frac{1}{2}i^2\frac{dL}{d\theta}}$$

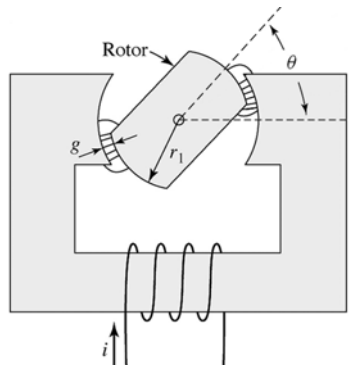$$P_{mech} = T_e \omega_r \qquad \omega_r = \frac{d\theta}{dt}$$

$$P_{mech} = \frac{1}{2}i^2\frac{dL}{dt}$$

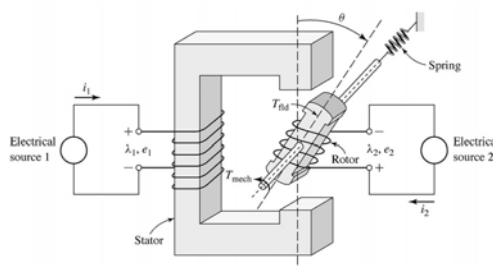**Ex:** The self inductance $L(\theta)$ in the figure as a function of rotor position is given by

$$L(\theta) = L_0 + L_2 \cos(2\theta)$$

where the stator current is $i(t) = I_m \sin(\omega t)$

(i) Obtain an expression for electromagnetic torque produced (instantaneous torque)

(ii) Let $\theta = \omega_r t + \theta_0$, find necessary condition for non-zero average torque

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(b) Doubly-excited device

$$\lambda_1 = L_1 i_1 + M i_2$$
$$\lambda_2 = L_2 i_2 + M i_1$$

$$\lambda_1 = L_1(\theta) i_1(t) + M(\theta) i_2(t)$$
$$\lambda_2 = L_2(\theta) i_2(t) + M(\theta) i_1(t)$$

$$e_1 = \frac{d\lambda_1}{dt} \qquad e_2 = \frac{d\lambda_2}{dt}$$

$$e_1 = L_1 \frac{di_1}{dt} + i_1 \frac{dL_1}{d\theta}\frac{d\theta}{dt} + M \frac{di_2}{dt} + i_2 \frac{dM}{d\theta}\frac{d\theta}{dt}$$

$$e_2 = L_2 \frac{di_2}{dt} + i_2 \frac{dL_2}{d\theta}\frac{d\theta}{dt} + M \frac{di_1}{dt} + i_1 \frac{dM}{d\theta}\frac{d\theta}{dt}$$

$$v_1 = e_1 + r_1 i_1 \qquad v_2 = e_2 + r_2 i_2$$

$$\omega_r = \frac{d\theta}{dt}$$

Terminal voltage equation (in matrix form):

$$\begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} r_1 & 0 \\ 0 & r_2 \end{bmatrix}\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} + \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix}\frac{d}{dt}\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} + \frac{d}{d\theta}\begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix}\begin{bmatrix} i_1 \\ i_2 \end{bmatrix}\omega_r$$
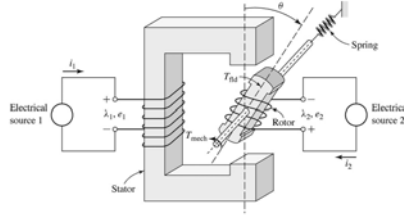
$$\begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} r_1 & 0 \\ 0 & r_2 \end{bmatrix}\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} + \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix}\frac{d}{dt}\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} + \frac{d}{d\theta}\begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix}\begin{bmatrix} i_1 \\ i_2 \end{bmatrix}\omega_r$$

Total power

$$v_1 i_1 + v_2 i_2 = \begin{bmatrix} i_1 & i_2 \end{bmatrix}\begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

$$v_1 i_1 + v_2 i_2 = I^T V = \underset{\substack{\uparrow \\ P_{elec}}}{I^T R I} + I^T L \frac{dI}{dt} + \underset{\substack{\uparrow \\ P_{cu}}}{I^T \frac{dL}{d\theta} I \omega_r} \quad \textbf{(in matrix form)}$$

Total electrical power input:

$$P_{elec} = \underbrace{i_1^2 r_1 + i_2^2 r_2}_{\text{Copper loss}} + \underbrace{L_1 i_1 \frac{di_1}{dt} + M i_1 \frac{di_2}{dt} + L_2 i_2 \frac{di_2}{dt} + M i_2 \frac{di_1}{dt} + i_1^2 \frac{dL_1}{d\theta}\omega_r + 2i_1 i_2 \frac{dM}{d\theta}\omega_r + i_2^2 \frac{dL_2}{d\theta}\omega_r}_{\text{Rate of increase in stored energy in MF + Electr.power converted to mech. en.}}$$

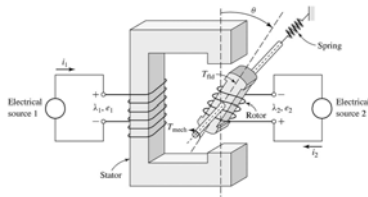
$$P_{elec} = i_1^2 r_1 + i_2^2 r_2 + L_1 i_1 \frac{di_1}{dt} + M i_1 \frac{di_2}{dt} + L_2 i_2 \frac{di_2}{dt} + M i_2 \frac{di_1}{dt} + i_1^2 \frac{dL_1}{d\theta}\omega_r + 2i_1 i_2 \frac{dM}{d\theta}\omega_r + i_2^2 \frac{dL_2}{d\theta}\omega_r$$

Magnetic stored energy

$$W_{fld} = \int i_1 d\lambda_1 + \int i_2 d\lambda_2$$

$$= \frac{1}{2}L_1 i_1^2 + \frac{1}{2}L_2 i_2^2 + M i_1 i_2$$

$$P_{fld} = \frac{dW_{fld}}{dt}$$

$$P_{fld} = L_1 i_1 \frac{di_1}{dt} + M i_1 \frac{di_2}{dt} + L_2 i_2 \frac{di_2}{dt} + M i_2 \frac{di_1}{dt} + \frac{1}{2}i_1^2 \frac{dL_1}{d\theta}\omega_r + \frac{1}{2}i_2^2 \frac{dL_2}{d\theta}\omega_r + i_1 i_2 \frac{dM}{d\theta}\omega_r$$
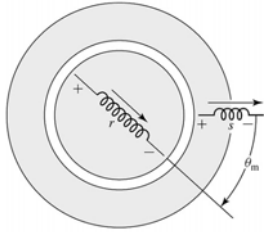
$$P_{mech} = P_{elec} - P_{cu} - P_{fld}$$

$$P_{mech} = \frac{1}{2}i_1^2 \frac{dL_1}{d\theta}\omega_r + \frac{1}{2}i_2^2 \frac{dL_2}{d\theta}\omega_r + i_1 i_2 \frac{dM}{d\theta}\omega_r \qquad P_{mech} = T_e \omega_r$$

$$T_e = \frac{1}{2}i_1^2 \frac{dL_1}{d\theta} + \frac{1}{2}i_2^2 \frac{dL_2}{d\theta} + i_1 i_2 \frac{dM}{d\theta} \qquad \textbf{In matrix form: } T_e = \frac{1}{2}I^T \frac{dL}{d\theta} I$$

Ex1: T_e?

Ex2: T_e?