## III. Three-Phase Circuits

## Three-Phase Systems

Almost all electric power generation and most of the power transmission in the world is in the form of three-phase AC circuits. A three-phase AC system consists of three-phase generators, transmission lines, and loads.

There are two major advantages of three-phase systems over a singlephase system:
a) More power per kilogram of metal form a three-phase machine;
b) Power delivered to a three-phase load is constant at all time, instead of pulsing as it does in a single-phase system.

The first three-phase electrical system was patented in 1882 by John Hopkinson - British physicist, electrical engineer, Fellow of the Royal Society.

## 1. Generation of three-phase voltages and currents

A three-phase generator consists of three singlephase generators with voltages of equal amplitudes and phase differences of $120^{\circ}$.


Each of three-phase generators can be connected to one of three identical loads.

This way the system would consist of three single-phase circuits differing in phase angle by $120^{\circ}$.

The current flowing to each load can be found as

$$
I=\frac{V}{Z}
$$

 $I=\frac{V}{Z}$


Therefore, the currents flowing in each phase are


$$
\begin{aligned}
& I_{A}=\frac{V \angle 0^{0}}{Z \angle \theta}=I \angle-\theta \\
& I_{B}=\frac{V \angle-120^{\circ}}{Z \angle \theta}=I \angle-120-\theta \\
& I_{A}=\frac{V \angle-240^{\circ}}{Z \angle \theta}=I \angle-240-\theta
\end{aligned}
$$

We can connect the negative (ground) ends of the three single-phase generators and loads together, so they share the common return line (neutral).


The current flowing through a neutral can be found as

$$
\begin{aligned}
I_{N} & =I_{A}+I_{B}+I_{C}=I \angle-\theta+I \angle-\theta-120^{\circ}+I \angle-\theta-240^{\circ} \\
& =I \cos (-\theta)+j I \sin (-\theta)+I \cos \left(-\theta-120^{\circ}\right)+j I \sin \left(-\theta-120^{\circ}\right)+I \cos \left(-\theta-240^{\circ}\right)+j I \sin \left(-\theta-240^{\circ}\right) \\
& =I\left[\cos (-\theta)+\cos \left(-\theta-120^{\circ}\right)+\cos \left(-\theta-240^{\circ}\right)\right]+j I\left[\sin (-\theta)+\sin \left(-\theta-120^{\circ}\right)+\sin \left(-\theta-240^{\circ}\right)\right] \\
& =I\left[\cos (-\theta)+\cos (-\theta) \cos \left(120^{\circ}\right)+\sin (-\theta) \sin \left(120^{\circ}\right)+\cos (-\theta) \cos \left(240^{\circ}\right)+\sin (-\theta) \sin \left(240^{\circ}\right)\right] \\
& +j I\left[\sin (-\theta)+\sin (-\theta) \cos \left(120^{\circ}\right)-\cos (-\theta) \sin \left(120^{\circ}\right)+\sin (-\theta) \cos \left(240^{\circ}\right)-\cos (-\theta) \sin \left(240^{\circ}\right)\right]
\end{aligned}
$$

which is simplified to be

$$
\begin{aligned}
I_{N} & =I\left[\cos (-\theta)-\frac{1}{2} \cos (-\theta)+\frac{\sqrt{3}}{2} \sin (-\theta)-\frac{1}{2} \cos (-\theta)-\frac{\sqrt{3}}{2} \sin (-\theta)\right] \\
& +j I\left[\sin (-\theta)-\frac{1}{2} \sin (-\theta)+\frac{\sqrt{3}}{2} \cos (-\theta)-\frac{1}{2} \sin (-\theta)-\frac{\sqrt{3}}{2} \cos (-\theta)\right] \\
& =0
\end{aligned}
$$

So, as long as the three loads are equal, the return current in the neutral is zero!

Such three-phase power systems (equal magnitude, phase differences of $120^{\circ}$, identical loads) are called balanced.

In a balanced system, the neutral is unnecessary!

Phase Sequence is the order in which the voltages in the individual phases peak.


## 2. Connection Types

There are two types of connections in three-phase circuits:
Y (Wye) and $\Delta$ (Delta)


Each generator and each load can be either $\mathbf{Y}$ - or $\boldsymbol{\Delta}$-connected. Any number of $\mathbf{Y}$ - and $\boldsymbol{\Delta}$-connected elements may be mixed in a power system.

Phase quantities - voltages and currents in a given phase.
Line quantities - voltages between the lines and currents in the lines connected to the generators.

## a) Y-connection

Assuming a resistive load...



The current in any line is the same as the current in the corresponding phase.

$$
I_{L}=I_{\phi}
$$

Voltages are:

$$
\begin{aligned}
V_{a b}= & V_{a}-V_{b}=V_{\phi} \angle 0^{\circ}-V_{\phi} \angle-120^{\circ}=V_{\phi}-\left(-\frac{1}{2} V_{\phi}-j \frac{\sqrt{3}}{2} V_{\phi}\right)=\frac{3}{2} V_{\phi}+j \frac{\sqrt{3}}{2} V_{\phi} \\
= & \sqrt{3} V_{\phi}\left(\frac{\sqrt{3}}{2}+j \frac{1}{2}\right)=\sqrt{3} V_{\phi} \angle 30^{\circ} \\
& V_{\boldsymbol{a} \boldsymbol{b}}=\sqrt{\mathbf{3}} V_{\phi} \angle \mathbf{3 0 ^ { \circ }} \quad \boldsymbol{V}_{\boldsymbol{b} \boldsymbol{c}}=\sqrt{\mathbf{3}} \boldsymbol{V}_{\boldsymbol{\phi}} \angle \mathbf{- 9 0 ^ { \circ }} \boldsymbol{V}_{\boldsymbol{c} \boldsymbol{a}}=\sqrt{\mathbf{3}} \boldsymbol{V}_{\boldsymbol{\phi}} \angle-\mathbf{2 1 0 ^ { \circ }}
\end{aligned}
$$

Magnitudes of the line-to-line voltages and the line-to-neutral voltages are related as:

$$
V_{L L}=\sqrt{3} V_{\phi}
$$

In addition, the line-to-line voltages are shifted by $30^{\circ}$ with respect to the phase voltages.

In a connection with $\boldsymbol{a b c}$ sequence, the voltage of a line leads the phase voltage by $30^{\circ}$ as shown in the figure.


## b) $\Delta$-connection

Assuming a resistive load...


$$
\begin{aligned}
& V_{a b}=V_{\phi} \angle 0^{0} \\
& V_{b c}=V_{\phi} \angle-120^{\circ} \\
& V_{c a}=V_{\phi} \angle-240^{\circ}
\end{aligned}
$$

$$
I_{a b}=I_{\phi} \angle 0^{0}
$$

$$
I_{b c}=I_{\phi} \angle-120^{\circ}
$$

$$
I_{c a}=I_{\phi} \angle-240^{\circ}
$$



Line-to-line voltage magnitudes are the same as the phase voltages.

$$
V_{L L}=V_{\phi}
$$

Currents are:

$$
\begin{aligned}
I_{a} & =I_{a b}-I_{c a}=I_{\phi} \angle 0^{0}-I_{\phi} \angle 240^{\circ}=I_{\phi}-\left(-\frac{1}{2} I_{\phi}+j \frac{\sqrt{3}}{2} I_{\phi}\right) \\
& =\frac{3}{2} I_{\phi}-j \frac{\sqrt{3}}{2} I_{\phi}=\sqrt{3} I_{\phi}\left(\frac{\sqrt{3}}{2}-j \frac{1}{2}\right)=\sqrt{3} I_{\phi} \angle-30^{\circ} \\
\boldsymbol{I}_{\boldsymbol{a}} & =\sqrt{\mathbf{3}} \boldsymbol{I}_{\boldsymbol{\phi}} \angle-\mathbf{3 0} \quad \boldsymbol{I}_{\boldsymbol{b}}=\sqrt{\mathbf{3}} \boldsymbol{I}_{\boldsymbol{\phi}} \angle-\mathbf{1 5 0} \quad \boldsymbol{I}_{\boldsymbol{c}}=\sqrt{\mathbf{3}} \boldsymbol{I}_{\boldsymbol{\phi}} \angle-\mathbf{2 7 0 ^ { \circ }}
\end{aligned}
$$

Magnitudes of the line and phase currents are related as:

$$
I_{L}=\sqrt{3} I_{\phi}
$$

In addition, the line currents are shifted by $30^{\circ}$ with respect to the phase currents.

For the connections with the $\boldsymbol{a b c}$ phase sequences, the current of a line lags the corresponding phase current by $30^{\circ}$ as shwon in the figure.


## Wye (Y) Connected Load



## Delta ( $\Delta$ ) Connected Load



## Practical Use

What do you want to use in practice?
[Most common usage]

- $\Delta$-connected loads are most common to allow easy addition and removal of loads in each phase
- Y-connected sources are most common to avoid circulating currents when there is a small imbalance.


## c) Power relationship

For a balanced $\mathbf{Y}$-connected load with the impedance $\mathbf{Z}_{\phi}=\mathbf{Z} \angle \theta$ and phase voltages as:

$$
\begin{aligned}
& v_{a n}(t)=\sqrt{2} V \sin \omega t \\
& v_{b n}(t)=\sqrt{2} V \sin \left(\omega t-120^{\circ}\right) \\
& v_{c n}(t)=\sqrt{2} V \sin \left(\omega t-240^{\circ}\right)
\end{aligned}
$$

The currents can be found as:

$$
\begin{aligned}
& i_{a}(t)=\sqrt{2} I \sin (\omega t-\theta) \\
& i_{b}(t)=\sqrt{2} I \sin \left(\omega t-120^{\circ}-\theta\right) \\
& i_{c}(t)=\sqrt{2} I \sin \left(\omega t-240^{\circ}-\theta\right)
\end{aligned}
$$



The instantaneous power is:

$$
p(t)=v(t) i(t)
$$

Therefore, the instantaneous power supplied to each phase is:


$$
\begin{aligned}
& p_{a}(t)=v_{a n}(t) i_{a}(t)=2 V I \sin (\omega t) \sin (\omega t-\theta) \\
& p_{b}(t)=v_{b n}(t) i_{b}(t)=2 V I \sin \left(\omega t-120^{\circ}\right) \sin \left(\omega t-120^{\circ}-\theta\right) \\
& p_{c}(t)=v_{c n}(t) i_{c}(t)=2 V I \sin \left(\omega t-240^{\circ}\right) \sin \left(\omega t-240^{\circ}-\theta\right)
\end{aligned}
$$

Simplify the above equations using $\sin \alpha \sin \beta=\frac{1}{2}[\cos (\alpha-\beta)-\cos (\alpha+\beta)]$

$$
\begin{aligned}
& p_{a}(t)=V I[\cos \theta-\cos (2 \omega t-\theta)] \\
& p_{b}(t)=V I\left[\cos \theta-\cos \left(2 \omega t-240^{\circ}-\theta\right)\right] \\
& p_{c}(t)=V I\left[\cos \theta-\cos \left(2 \omega t-480^{\circ}-\theta\right)\right]
\end{aligned}
$$

The total power on the load is given by

$$
p_{t o t}(t)=p_{a}(t)+p_{b}(t)+p_{c}(t)=3 V I \cos \theta
$$

The pulsing components cancel each other because of $120^{\circ}$ phase shifts, so the total power on the load is constant.

The figure shows:
a) The instantaneous power in each phase.
b) The total power supplied to the load (which is constant)


Phase quantities in each phase of a $\mathbf{Y}$ - or $\boldsymbol{\Delta}$-connection.

$$
\text { Real Power: } \quad P=3 V_{\phi} I_{\phi} \cos \theta=3 I_{\phi}{ }^{2} Z \cos \theta
$$

Reactive Power: $\quad Q=3 V_{\phi} I_{\phi} \sin \theta=3 I_{\phi}{ }^{2} Z \sin \theta$

Apparent Power: $\quad S=3 V_{\phi} I_{\phi}=3 I_{\phi}{ }^{2} Z$

NOTE: These equations are valid for balanced loads only.

Deriving line quantities of a $\mathbf{Y}$-connection.

Power consumed by a load: $P=3 V_{\phi} I_{\phi} \cos \theta$

$$
\begin{array}{ll}
\text { since for this load } & I_{L}=I_{\phi} \text { and } V_{L L}=\sqrt{3} V_{\phi} \\
\text { therefore } & P=3 \frac{V_{L L}}{\sqrt{3}} I_{L} \cos \theta
\end{array}
$$

Finally

$$
P=\sqrt{3} V_{L L} I_{L} \cos \theta
$$

NOTE: These equations are valid for balanced loads only.

Deriving line quantities of a $\Delta$-connection.

Power consumed by a load: $P=3 V_{\phi} I_{\phi} \cos \theta$

$$
\begin{aligned}
& \text { since for this load } I_{L}=\sqrt{3} I_{\phi} \text { and } V_{L L}=V_{\phi} \\
& \text { therefore } \\
& P=3 \frac{V_{L L}}{\sqrt{3}} I_{L} \cos \theta
\end{aligned}
$$

Finally

$$
P=\sqrt{3} V_{L L} I_{L} \cos \theta
$$

Same as for a $\mathbf{Y}$-connected load!
NOTE: These equations are valid for balanced loads only.

Line quantities for a $\mathbf{Y}$ - or $\Delta$-connection.

Real Power: $\quad P=\sqrt{3} V_{L L} I_{L} \cos \theta$

Reactive Power: $\quad Q=\sqrt{3} V_{L L} I_{L} \sin \theta$

Apparent Power: $S=\sqrt{3} V_{L L} I_{L}$

Reminder: $\theta$ is the load (or impedance) angle, i.e. the angle between the phase voltage and the phase current.

NOTE: These equations are valid for balanced loads only.

## d) Analysis of balanced systems

A $\boldsymbol{\Delta}$-connected circuit can be analyzed via the transform of impedances by the Y- $\boldsymbol{\Delta}$ transform. For a balanced load, it states that a $\Delta$-connected load consisting of three equal impedances $\mathbf{Z}$ is equivalent to a $\mathbf{Y}$-connected load with the impedances $\mathbf{Z} / 3$.

This equivalence implies that the voltages, currents, and powers supplied to both loads would be the same.


Ex. For a 208-V three-phase ideally balanced system shown below, Find:
a) The magnitude of the line current $I_{L}$
b) The magnitude of the load's line and phase voltages $V_{L L}$ and $V_{\phi L}$;
c) The real, reactive, and the apparent powers consumed by the load;
d) The power factor of the load.


Both, the generator and the load are Yconnected, therefore, it's easy to construct a per-phase equivalent circuit.

a) Phase current:

$$
I_{L}=\frac{V}{Z_{L}+Z_{\text {load }}}=\frac{120 \angle 0^{0}}{(0.06+j 0.12)+(12+j 9)}=\frac{120 \angle 0^{0}}{12.06+j 9.12}=\frac{120 \angle 0^{0}}{15.12 \angle 37.1^{0}}=7.94 \angle-37.1^{0} \quad \mathrm{~A}
$$

b) Phase voltage over the load:

$$
V_{\phi L}=I_{\phi L} Z_{\phi L}=\left(7.94 \angle-37.1^{0}\right)(12+j 9)=\left(7.94 \angle-37.1^{0}\right)\left(15 \angle 36.9^{0}\right)=119.1 \angle-0.2^{0} V
$$

and the maignitude of the line voltage on the load:

$$
V_{L L}=\sqrt{3} V_{\phi L}=206.3 \mathrm{~V}
$$

c) The real power consumed by the load:

$$
P_{\text {load }}=3 V_{\phi} I_{\phi} \cos \theta=3 \cdot 119.1 \cdot 7.94 \cos 36.9^{\circ}=2270 \mathrm{~W}
$$

The reactive power consumed by the load:


$$
Q_{\text {load }}=3 V_{\phi} I_{\phi} \sin \theta=3 \cdot 119.1 \cdot 7.94 \sin 36.9^{0}=1702 \mathrm{var}
$$

The apparent power consumed by the load:

$$
S_{\text {load }}=3 V_{\phi} I_{\phi}=3 \cdot 119.1 \cdot 7.94=2839 \mathrm{VA}
$$

d) The load power factor:

$$
P F_{\text {load }}=\cos \theta=\cos 36.9^{\circ}=0.8-\text { lagging }
$$

## e) One-line diagrams

Since, in a balanced system, three phases are similar except of the $120^{\circ}$ phase shift, power systems are frequently represented by a single line showing all three phases of the real system.


This is a one-line diagram.
Such diagrams usually include all the major components of a power system: generators, transformers,
 transmission lines, loads.

If we can neglect the impedance of the transmission line, an important simplification in the power calculation is possible...

If the generator voltage in the system is known, then we can find the current and power factor at any point in the system as follows:

1. The line voltages at the generator and the loads will be identical since the line is lossless.
2. Real and reactive powers on each load.
3. The total real and reactive powers supplied to all loads from the point examined.
4. The system power factor at that point using the power triangle relationship.
5. Line and phase currents at that point.

We can treat the line voltage as constant and use the power triangle method to quickly calculate the effect of adding a load on the overall system and power factor.

